



March 7th, 2005

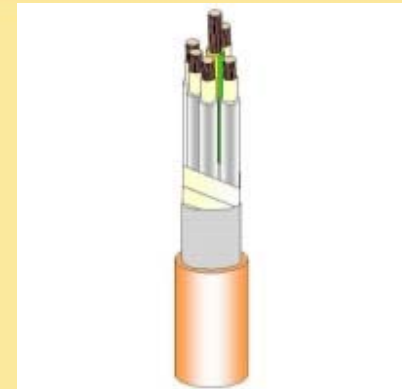
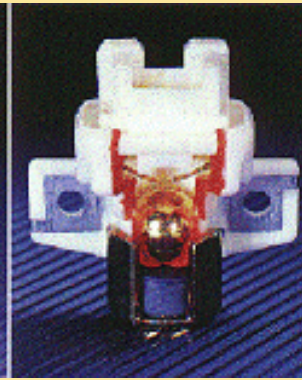
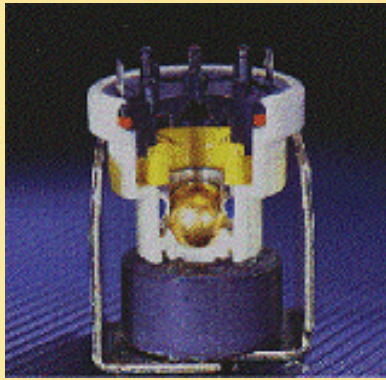
Properties of the insulators: Influence of the electrical charges

presented by Christelle GUERRET

Chargée de recherche du CNRS

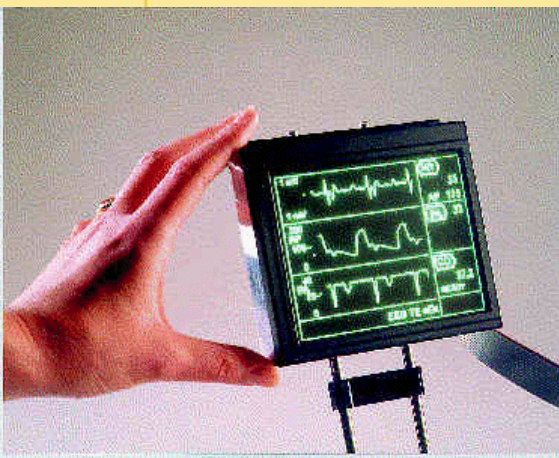
to obtain the "Habilitation à Diriger des Recherches"





Electromechanical sensor of acceleration for airbag Spatial vehicles

Insulators for cables



FEG screen

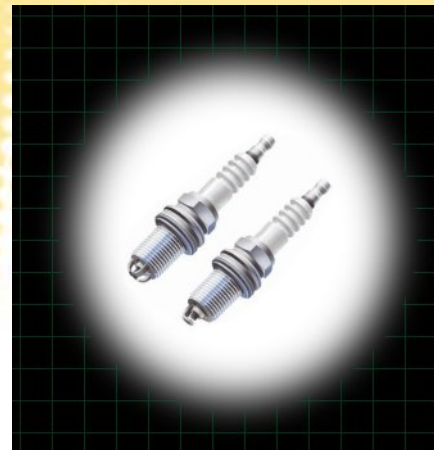
What role for the electrical charges ?



Extrusion of polymers



yarn-guide



Sparking plug



Pieces for mitigation tap



OUTLINE

- I. Examples of industrial applications for the insulators: Evidencing of the role of the electrical charges.**
 1. Modification of friction and adhesion
 2. Flow and trapping of the electrical charges.

- II. Contribution of the electrostatic forces to the adhesion of the materials:**

- III. Characterization of the properties of charges flow and charges trapping: SEMM method and simulations**

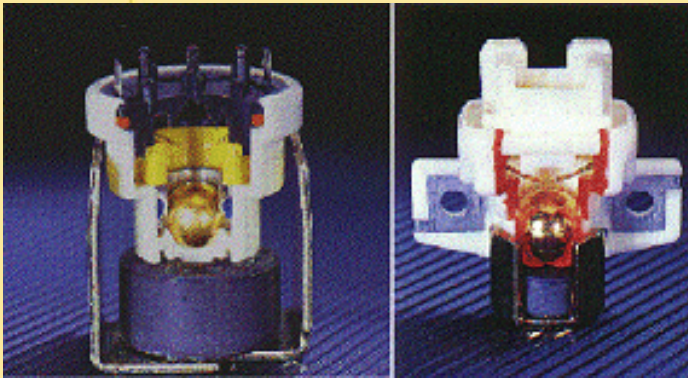
- IV. Conclusions and Prospects**

I.1. Modification of friction and adhesion

Electro-mechanical sensor of acceleration for air-bag

Principle :

- metallic ball in an insulator guide
- maintained by a magnetic field
- during a strong acceleration the ball overcome the magnetic field and establish electrical contact .



utilization → triboelectrification against the guide → ball stucked on the guide wall

**Inactivation of the sensor
because of the adhesion of the
ball on the insulating guide wall**

**Fundamental study of the interaction
between a charged metallic ball and an
insulating plane**

**Usefulness of the comprehension of the
triboelectrification phenomenon**

ACI* (Tribosurfélec)

I.1. Modification of friction and adhesion

Pieces for mitigation tap

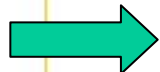


Principe :

- simultaneous control of the flow and of the temperature of water
- superposition of the holes of both ceramic disks
- sliding one over the second during the use

utilization → friction of the two disks → sticking of the two disks

unusable tap due to the
adhesion of the two ceramic
disks



Usefulness of the comprehension of the triboelectrification phenomenon between two similar materials

ACI* (Tribosurfélec)

I.2. Transport and trapping of the electrical charges

yarn-guide for textile industries



Performances:

- strength to abrasion
- strength to chemical corrosion
- high mechanical characteristics
- used materials : Al_2O_3 , $\text{Al}_2\text{O}_3+\text{Zr}$, TiO_2

Yarn adhere to the yarn-guide
during the use when the
friction coefficient is too high

Previous study*:

link between the friction coefficient and the ability of the material to trap charges

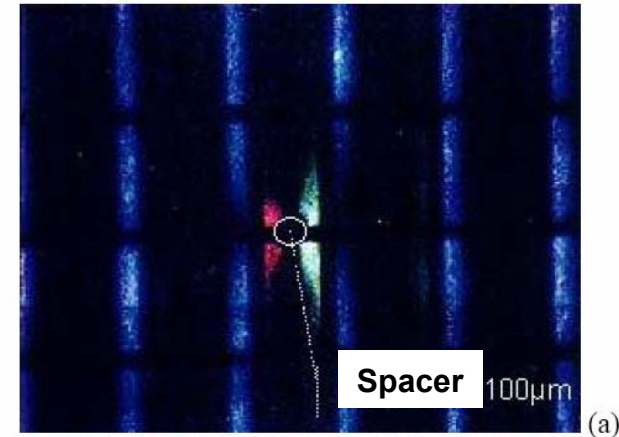
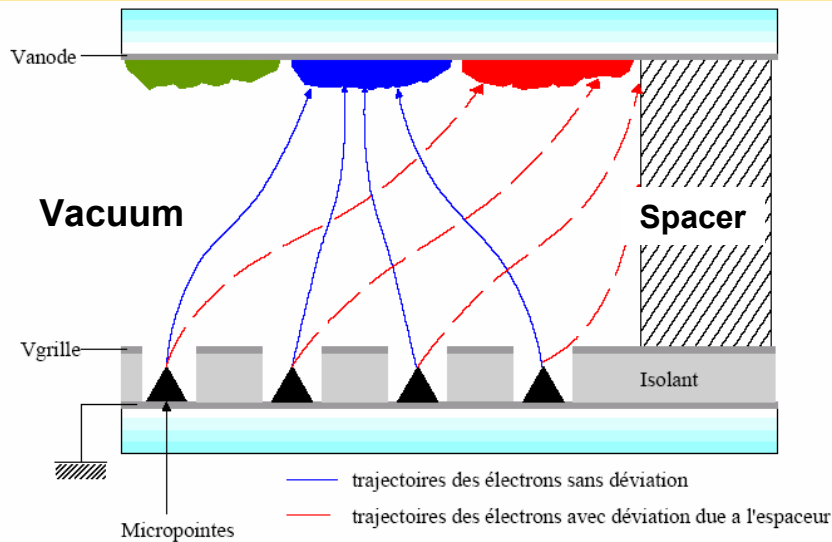


Importance of the ability of the material to trap charges : study of TiO_2

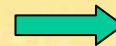
ACI
Thèse T. Temga

I.2. Transport and trapping of the electrical charges

FEG flat screen *



Problem of "mixing" of the colors due to the electrostatic fields created by the charging of the spacers



Definition of "trapping insulators" and "conductive insulators"*



Characterization of the behavior of dielectrics under electronic irradiation: transport and trapping of charges...

* D. Braga, Mémoire de Thèse, Université Paris XI, 2003.

** T. Thome, D. Braga, G. Blaise, *J. Appl. Phys.*, 2004, 95 (5), 2619 .

I.2. Transport and trapping of the electrical charges

Sparking plugs

Conditions of use :

- corrosive medium
- strong variations of temperature and pressure
- high voltage
- miniaturization



Aging of the materials

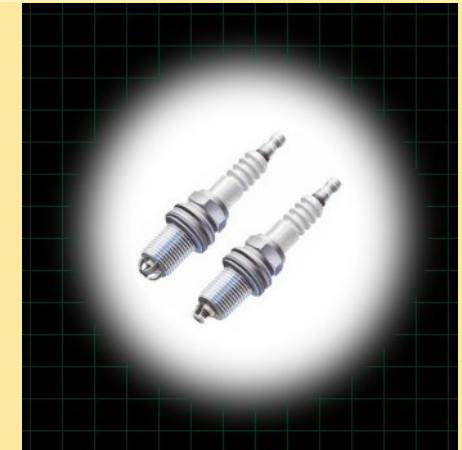
Strength to dielectric breakdown in different ranges of temperature



Dielectric breakdown of the sparking plugs



Transport and trapping of charges...
Links with the dielectric rigidity of insulators
Behavior under aging and temperature variations ...



Applications:

- motorbike
- automobiles
- boats
- rockets...

Thèse X. Meyza*
Thèse M. Touzin*

OUTLINE

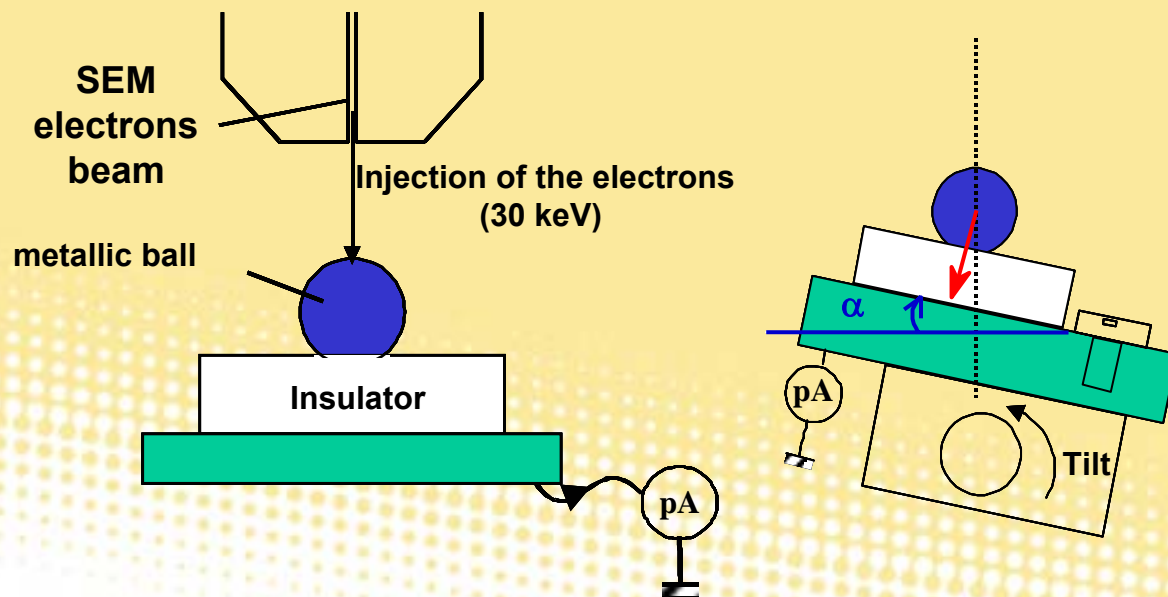
- II. **Contribution of the electrostatic forces to the adhesion of the materials:**
 - 1. **Example of the charged metallic ball on an insulating plane**
 - 2. **Triboelectrification between two similar materials**

II.1. Charged metallic ball on an insulating plane

Experiences

Objectives of the study:

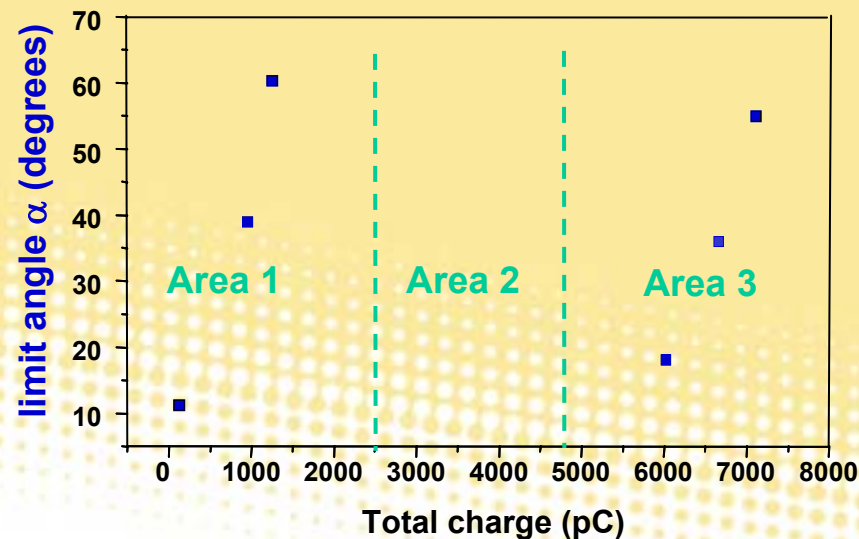
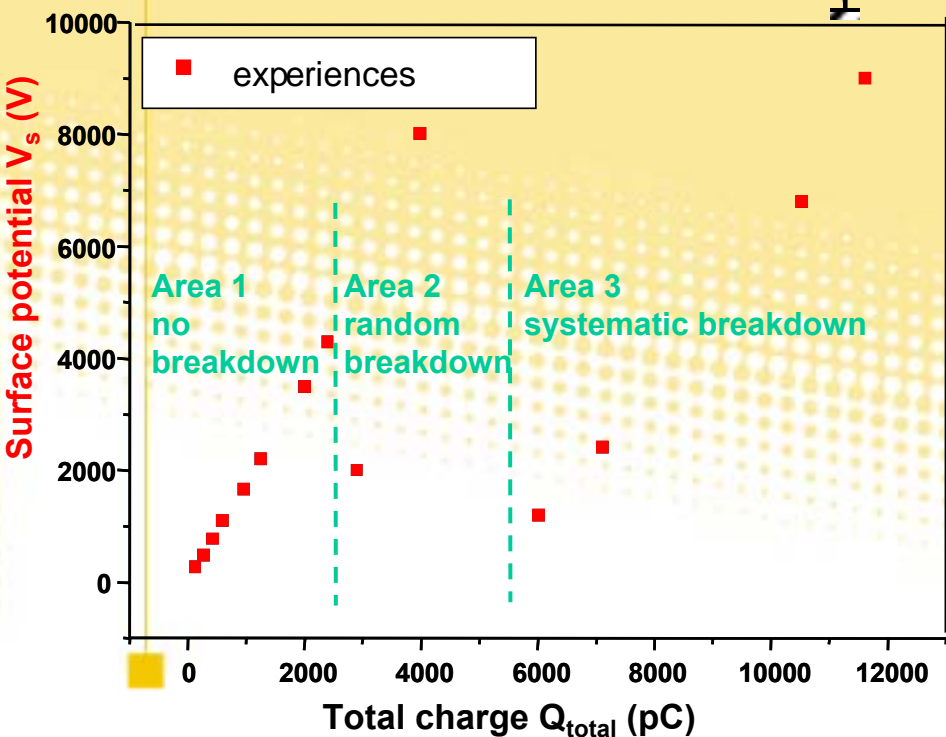
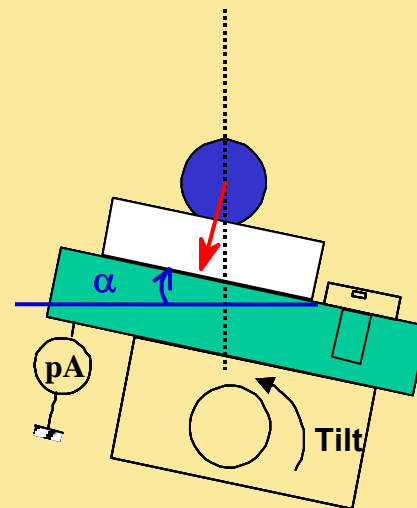
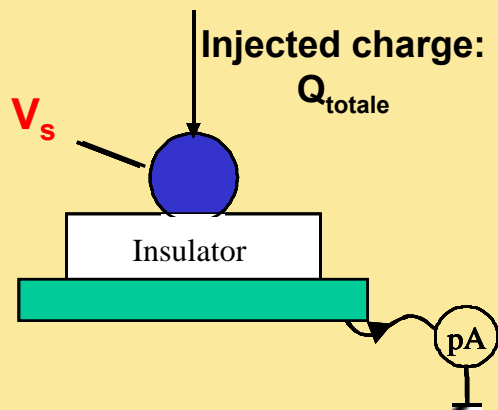
- evidencing of the strength of electrostatic forces
- "soft" injection of the electrical charges in an insulator ?



$$\sin\alpha - k\cos\alpha = \frac{k}{mg} F$$

II.1. Charged metallic ball on an insulating plane

Experiences



II.1. Charged metallic ball on an insulating plane

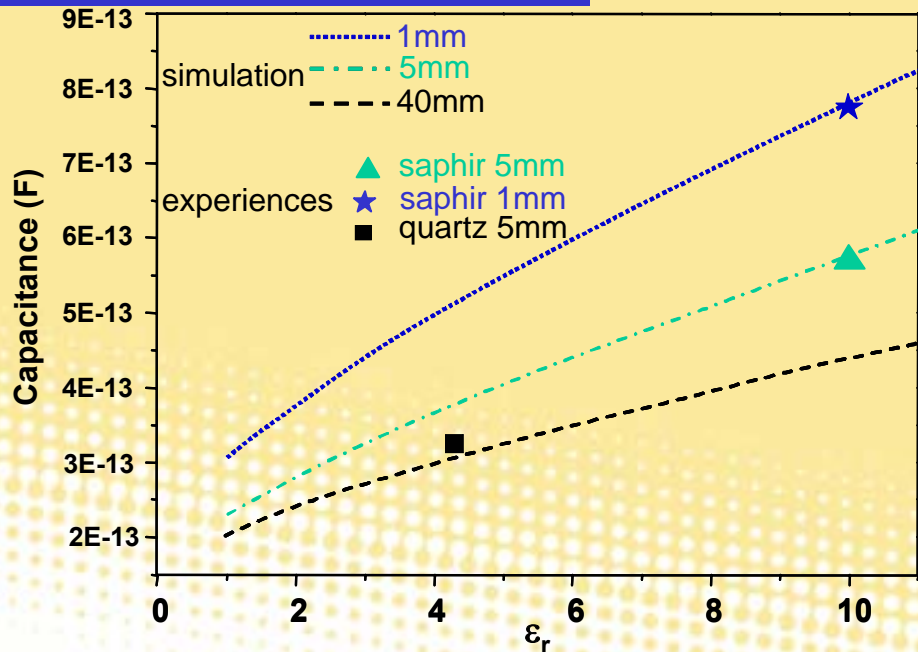
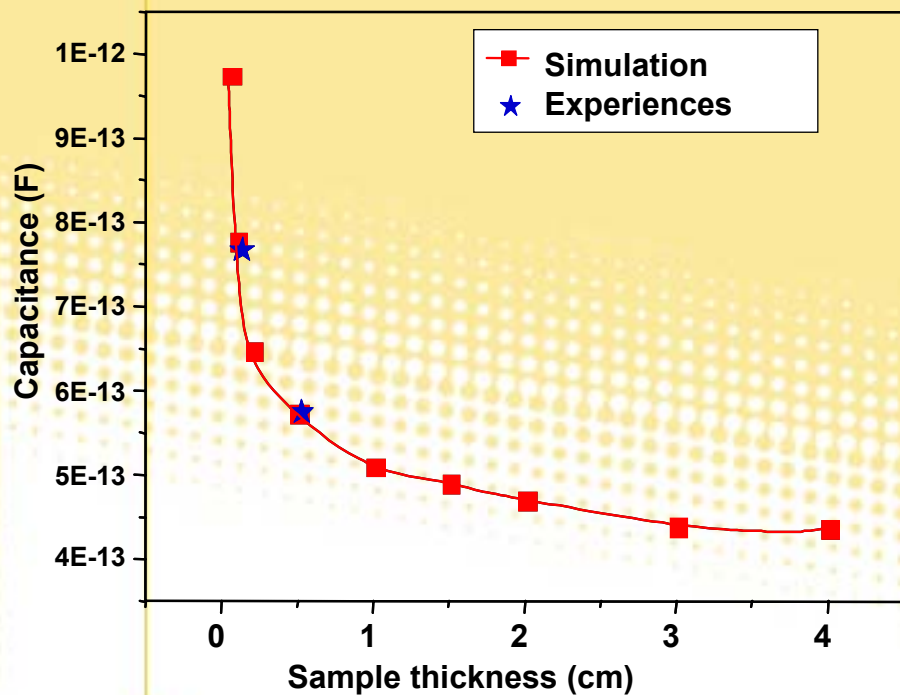
Simulations (Flux 2D)

Numerical Model* :

- axial symmetry, charge in the ball Q_i , potential V_s
- ball on an insulating disk (ϵ_r) thickness h ($R=20\text{mm}$)
- insulator on a grounded metallic plane plan



$$Q_i = C V_s$$



Influence of the sample holder

Dominant role of ϵ_r

* collaboration with N Burais, CEGELY, EC Lyon

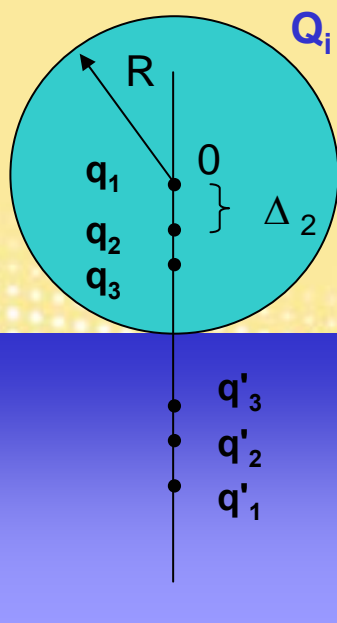
II.1. Charged metallic ball on an insulating plane

Analytical approach

Hypothesis of the calculation:

- conducting ball held on a semi-infinite dielectric
- case (a): charged sphere Q_i , non charged plane
- case (b): charged sphere Q_i , charged plane Q_t
- Q_t ponctual charge

Case (a) non charged plane: 2 infinite series of image charges



$$\left\{ \begin{aligned} q_{i+1} &= A^i * q_1 * \frac{1}{i+1} \\ q'_i &= -A^i * q_1 * \frac{1}{i} \\ \Delta_{i+1} &= \frac{i}{i+1} R \end{aligned} \right.$$

$A = (\epsilon_r - 1) / (\epsilon_r + 1)$
 due to the interface vacuum/dielectric

Δ_i = distance q_i - center O
 q'_i symmetric of q_i / interface

$$q_1 = \frac{-A}{\ln(1-A)} * Q_i$$

$$V_s = \sum_{i=1}^{\infty} \frac{q_i}{4\pi\epsilon_0 * (R - \Delta_i)} = - \frac{1}{4\pi\epsilon_0 R} \frac{A}{\ln(1-A)} Q_i$$

$$F = \frac{1}{4\pi\epsilon_0} \sum_i \sum_j \frac{q_i q_j}{(2R - \Delta_i - \Delta_j)^2} = \frac{1}{4\pi\epsilon_0 R^2} \left(\frac{A}{\ln(1-A)} \right)^2 * Q_i^2 * K_\epsilon$$

Capacitance C

$$K_\epsilon = \sum_i \sum_j A^{(i+j)-1} \frac{ij}{(i+j)^2}$$

sapphire ($\epsilon_r=10$) $K_\epsilon=4.69$, quartz ($\epsilon_r=4.3$) $K_\epsilon=0,91$

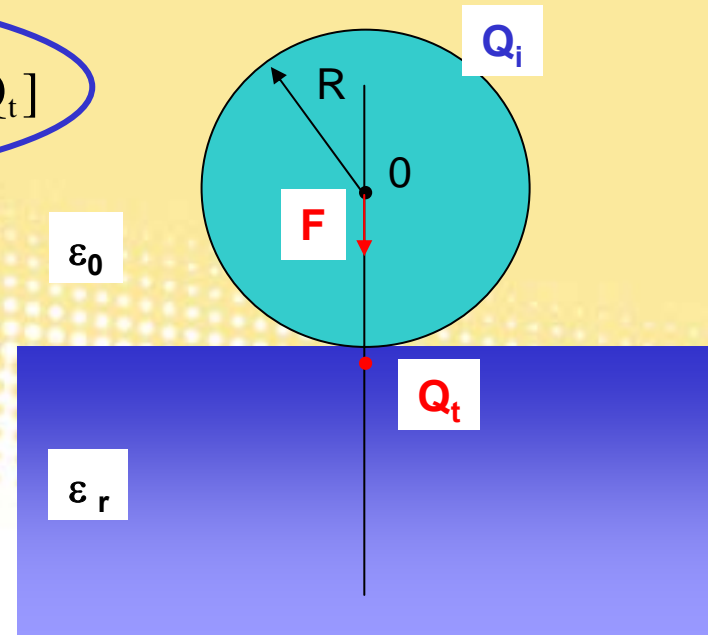
II.1. Charged metallic ball on an insulating plane

Analytical approach

Case (b) charged plane Q_t : 4 infinite series of image charges

$$V_s = \sum_{i=1}^{\infty} \frac{q_i}{4\pi\epsilon_0 * (R - \Delta_i)} + \sum_{i=1}^{\infty} \frac{q_i^d}{4\pi\epsilon_0 * (R - \Delta_i^d)} = -\frac{1}{4\pi\epsilon_0 R} \left[\frac{-A}{\ln(1-A)} Q_i + \frac{2}{\epsilon_r + 1} Q_t \right]$$

$$F = \frac{1}{4\pi\epsilon_0 R^2} \left[\left(\frac{A}{\ln(1-A)} \right)^2 * Q_i^2 * K_\epsilon - \frac{2}{\epsilon_r + 1} * Q_i * Q_t \right]$$



II.1. Charged metallic ball on an insulating plane

Analytical approach

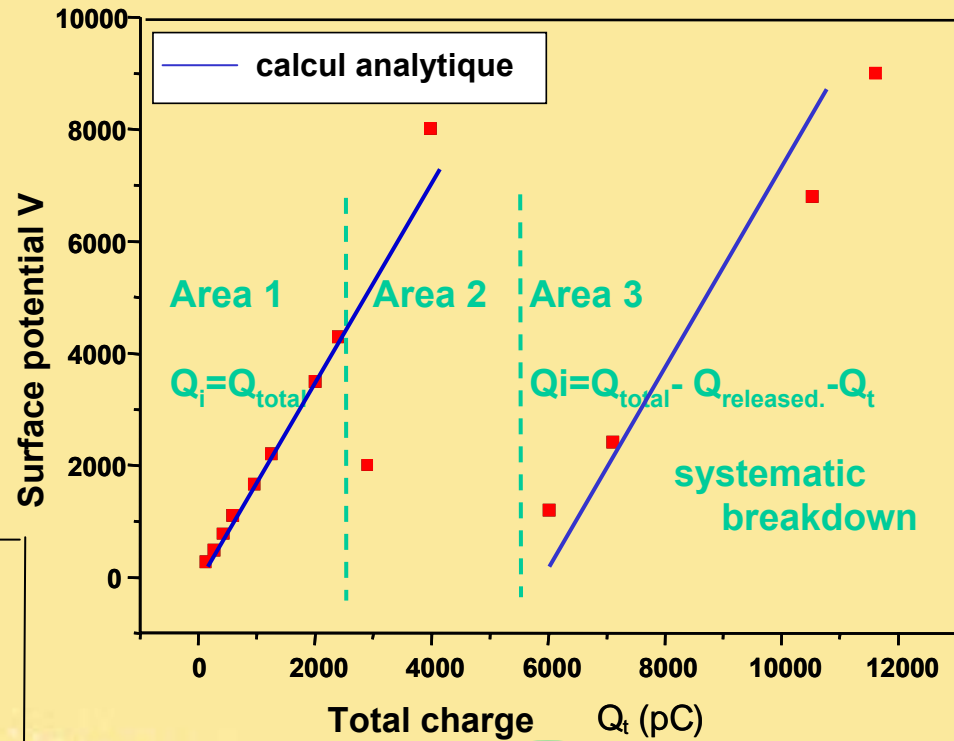
Area 1: $Q_i = Q_{\text{totale}}$

Area 2: Random breakdown

Area 3: $Q_i = Q_{\text{total}} - Q_{\text{released}} - Q_t$

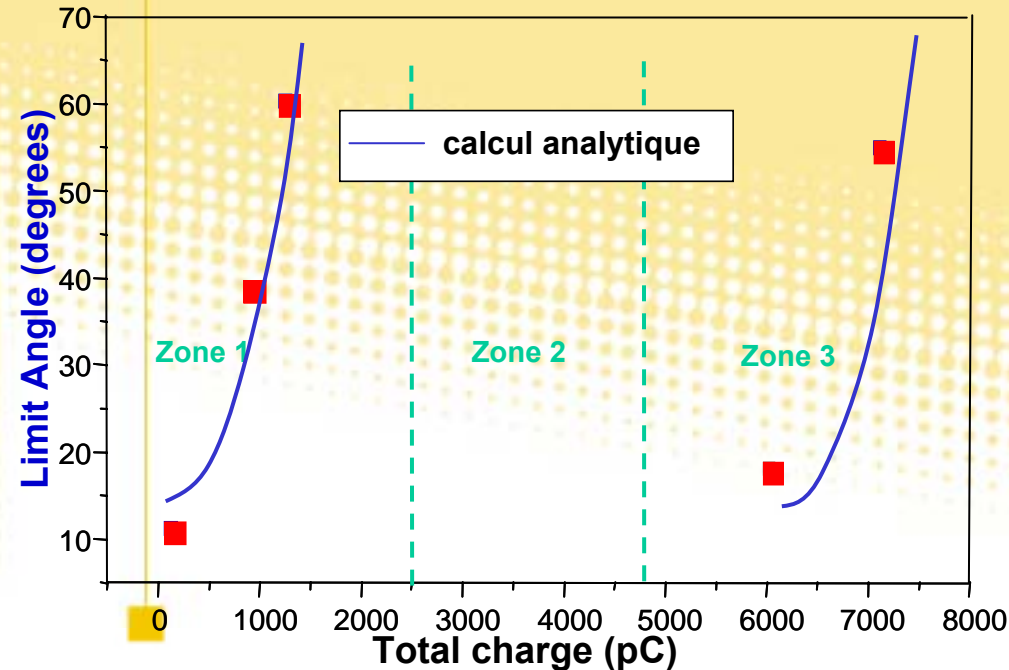
Systematic breakdown

($Q_{\text{released}} = 6000 \text{ pC}$, $Q_{\text{injected}} = 200 \text{ pC}$)



$$V_s = \frac{1}{4\pi\epsilon_0 R} \frac{A}{\ln(1-A)} Q_i$$

$$F = \frac{1}{4\pi\epsilon_0 R^2} \left(\frac{A}{\ln(1-A)} \right)^2 * Q_i^2 * K_\epsilon$$



II.1. Charged metallic ball on an insulating plane



Summ up*

Applicative results:

Adhesion of the ball is an electrostatic phenomenon

$$F_{\text{électrost}} = \frac{1}{4\pi\epsilon_0 R^2} \left(\frac{A}{\ln(1-A)} \right)^2 * Q_i^2 * K_\epsilon = \frac{C_{te}}{4\pi\epsilon_0 R^2} Q_i^2$$

sapphire ($\epsilon_r=10$), $C_{te} = 1,08$
 quartz ($\epsilon_r=4.3$) $C_{te} = 0,36$



Choice of the dielectric: nature, thickness
Dimensions of the ball

Fundamental results:

Mechanism of the ball-plane interaction under electronic injection: 3 steps

- 1- Small quantities of charges injected in the ball: all the charges stay in the sphere
- 2- Breakdown of the surrounding medium , Release of the charges present in the ball.
- 3- Systematic breakdown coupled with partial injection in the insulating plane and followed by a recovery of the injection in the ball

Remarks:

- stable volume trapping
- unusable for a "soft" injection

* C. Guerret, D. Juvé, D. Tréheux, N. Burais *Journal of Applied Physics* , Vol 92 (12), p 7425, 2002

- II. Contribution of the electrostatic forces to the adhesion of the materials:**
- 1. Example of the charged metallic ball on an insulating plane**
 - 2. Triboelectrification between two similar materials**

II.2. Triboelectrification between two similar materials

Position of the problem *



- **Triboelectrification between 2 different materials:** well-known mechanism in the case of two metals , no clear mechanism as soon as one of the material is an insulator
- **Triboelectrification between 2 similar materials:** not understood, not evidenced at the microscopic scale
- **Numerous studies, due to recent development of the apparatus (SFA, AFM, EFM)**

* C. Guerret, S. Bec, D. Tréheux, C.-R. de l'Académie des Sciences. Paris, t2, Série IV, p. 1-14 2001

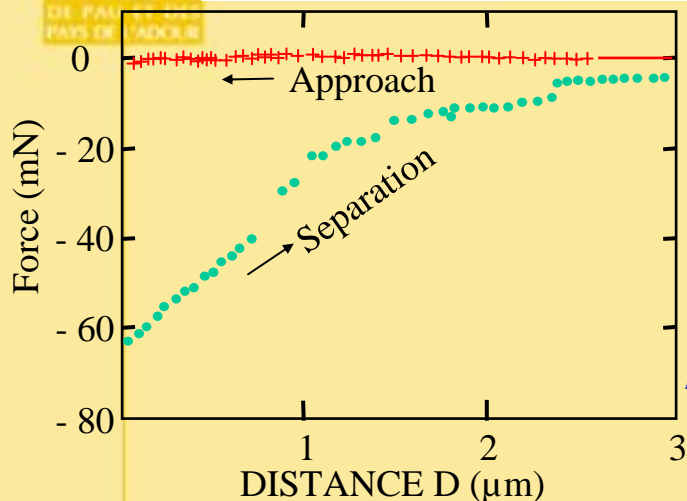
II.2. Triboelectrification between two similar materials



Results of the literature

Suface Force Apparatus : Mica/Silica, in dried N₂

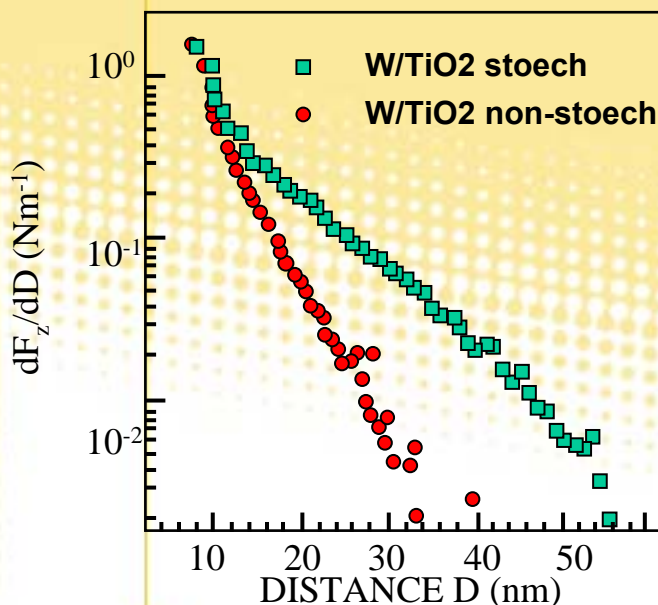
Horn R.G. and Smith D.T *Science* 256, (1992)



- attraction at long distance (>3 μm)
- density of the electrical charges: 10 mC/m²

AFM: Tungstene/ TiO₂ stoech. or non/stoech, Ultravacuum

Sounilhac S., Barthel E., Creuzet F. , *J. Appl. Phys.*, 85 (1) (1999)



- <15nm : van der Waals forces are dominant
- >15nm: Electrostatic forces for TiO₂ stoech
- density of the electrical charges : 10⁻³ mC/m²

AFM: Stability of charges in thin layer of Al₂O₃.

N. Felidj, J. Lambert, C. Guthmann, M. Saint Jean *Eur. Phys. J. A. P.* 12 (2000)

J. Lambert, C. Guthmann, M. Saint Jean *J. Appl. Phys.*, 93 (9) (2003)

- deposit of charges on the oxyde surfaces, by application of a potential or by friction
- density of the electrical charges : 10⁻⁵ mC/m²

II.2. Triboelectrification between two similar materials

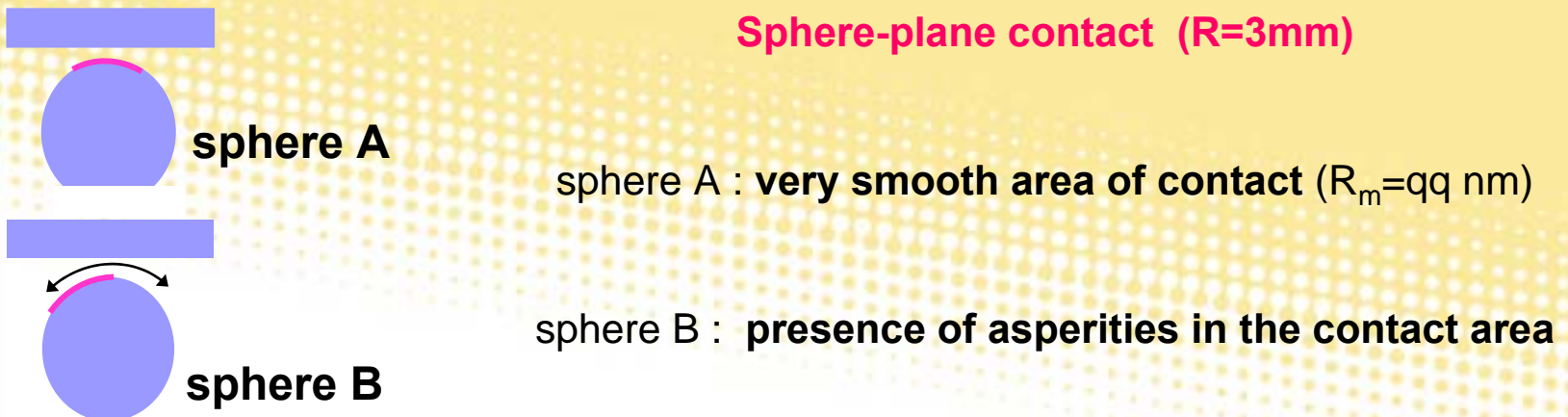
Adhesion between two similar insulating surfaces*

OBJECTIVE :

- Evidencing of the triboelectrification between two **similar materials**
- Characterization of the contribution of the **resulting electrostatic force** on the **adhesion**

EXPERIENCE :

- **Surface Force Apparatus of Ecole Centrale de Lyon (SFA)**
- **2 antagonists in monocrystalline alumina (sapphire)**



* Action Concertée Incitative, " Tribosurfélec" , collaboration IFoS- LTDS

** C. GUERRET-PIECOURT, J. VALLAYER, D. TREHEUX Wear, Vol 254, p 950-958, 2003

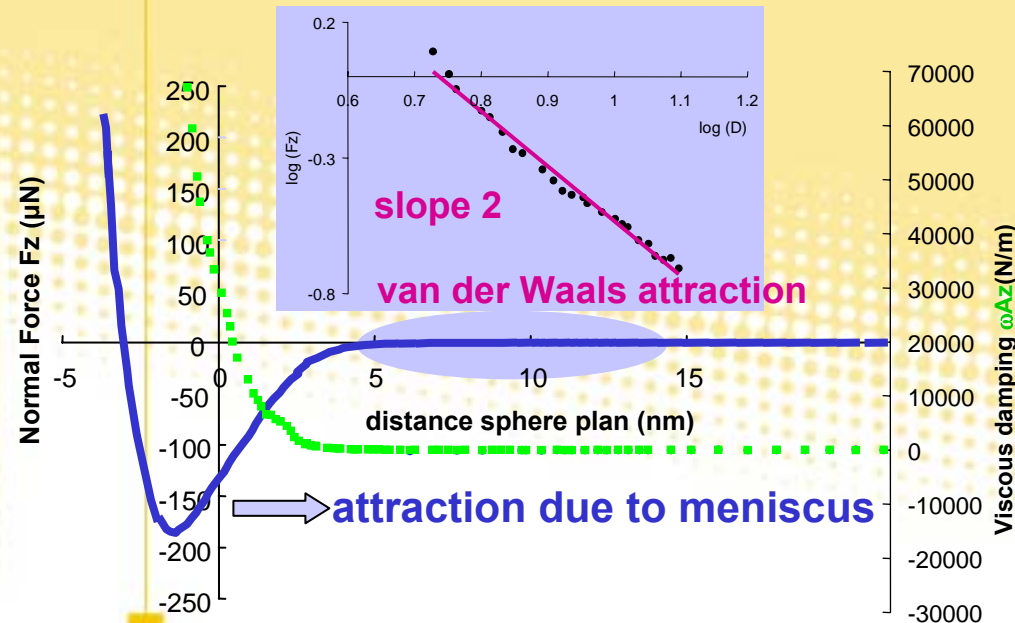
II.2. Triboelectrification between two similar materials

Case of the smooth sphere A

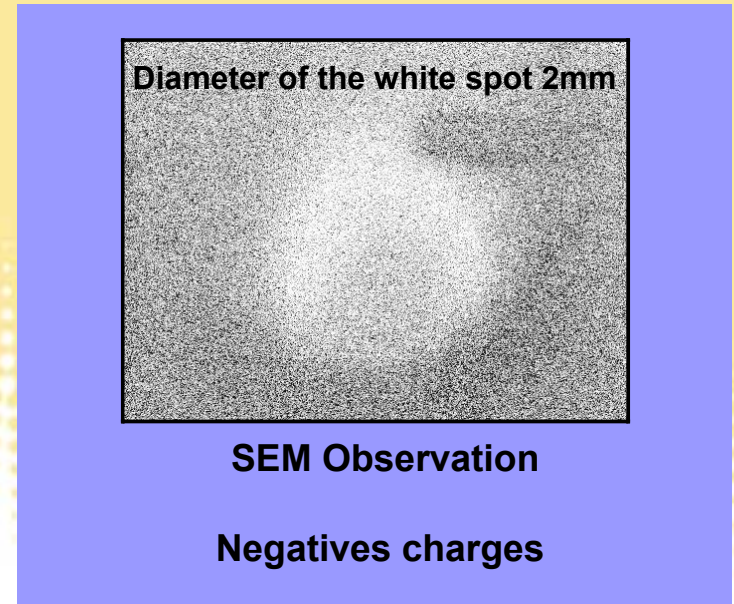
- **Before friction:**
 - attraction due to **van der Waals forces**
 - apparition of a viscous **damping** due to the formation of a water meniscus
- ➔ vacuum non suffisant to remove the remaining water

$$\frac{F_z}{R} = \frac{-A}{6D^2}$$

- **After friction:** - apparition of a **long distance force**, electrostatic charges



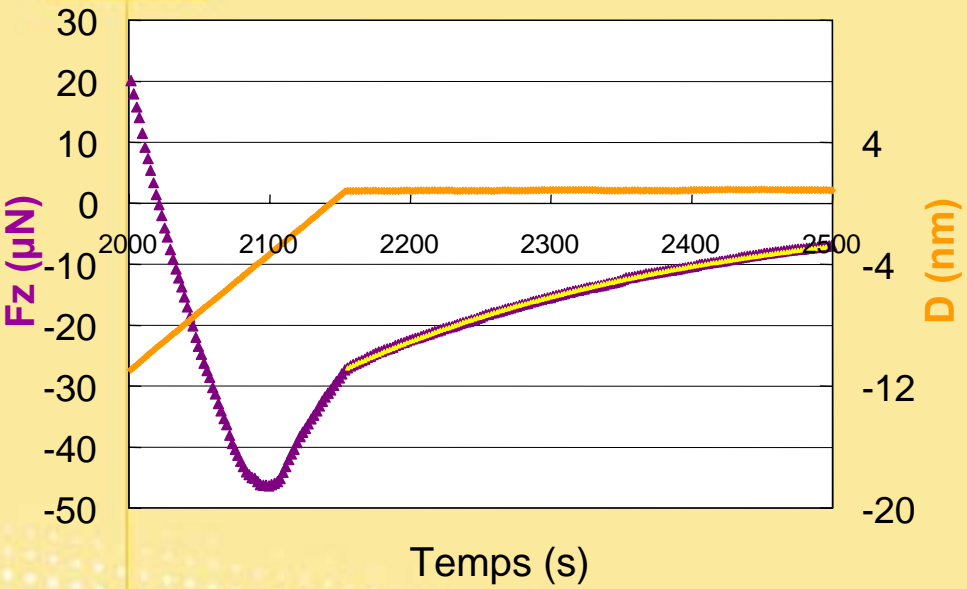
Before friction



After friction

II.2. Triboelectrification between two similar materials

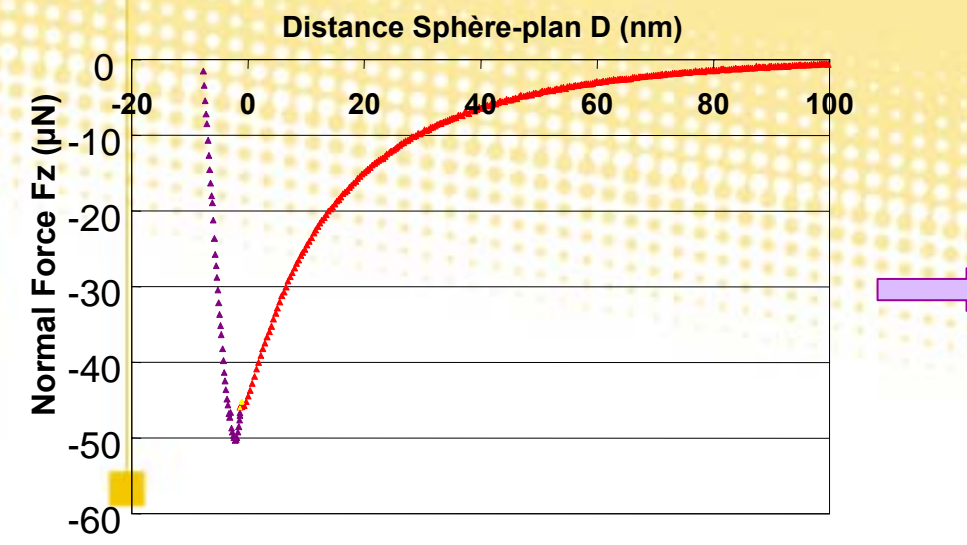
Case of the sphere B : attraction after friction



Stop of the unloading, at imposed distance :
attraction decreases with time

$$Fz = F_o \exp\left(-\frac{(t - t_o)}{\tau}\right)$$

$\tau = 256 \text{ s}$



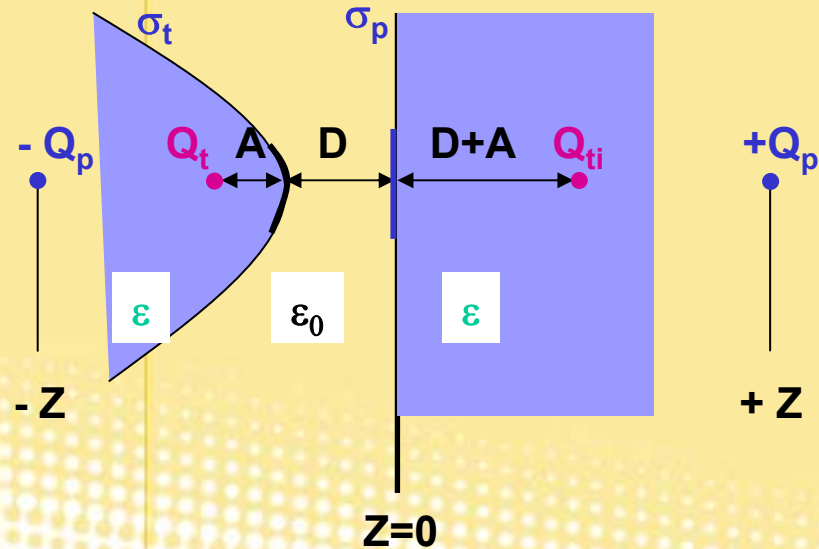
Specific way to measure the force during a small time of unloading (some s) :
attraction decreases with distance

II.2. Triboelectrification between two similar materials

Attraction after friction : Model of Burnham & al

Model of Burnham, Colton et Pollock (BCP)

Burnham N.A., Colton R.J., Pollock H.M., *Phys. Rev. Lett.* vol 69, n°1 (1992)



1st term:
 • due to the vacuum/dielectric interface
 • always attractive

2nd term:
 • depends on the signs of Q_t and Q_p
 • even if Q_t and Q_p have the same sign, at low distance the first term dominates

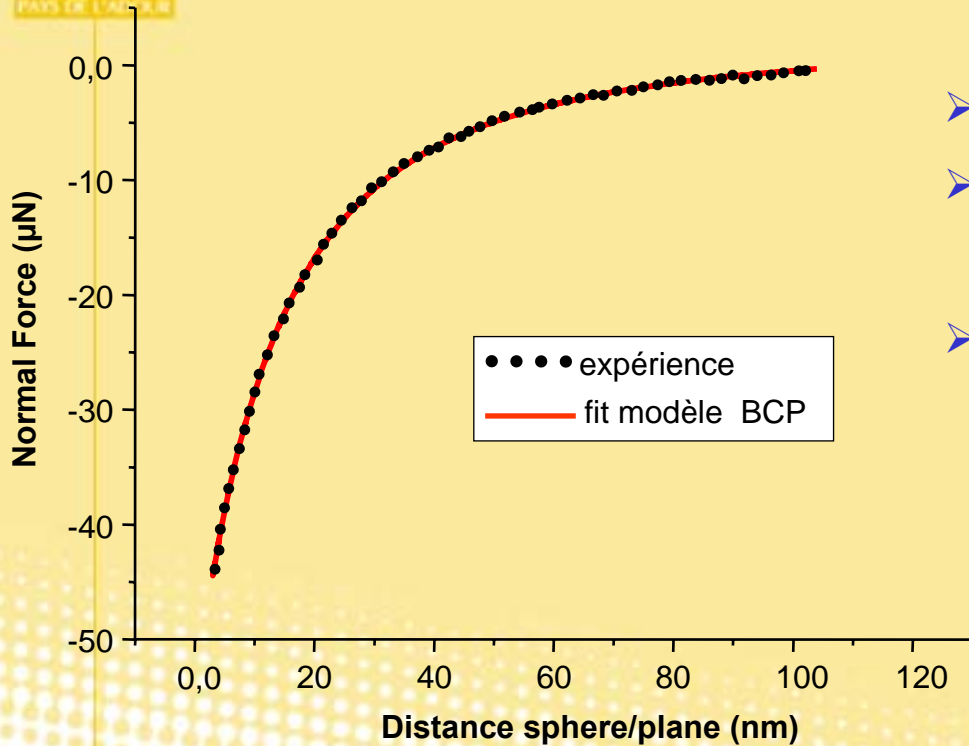
In our case :

$$4\pi\epsilon_0 F = - \frac{Q_t^2}{4(D+A)^2} \left(\frac{\epsilon - 1}{\epsilon + 1} \right) + \frac{RQ_tQ_p}{z(2D+A+R)^2} \left(\frac{\epsilon - 1}{\epsilon + 1} \right)^2$$

$\epsilon = 10$ for Al_2O_3

II.2. Triboelectrification between two similar materials

Attraction after friction : Model of Burnham & al



➤ Sapphire-sapphire friction

➤ Best fit between 0 and 100 nm :

• Charges of the même signe

➤ Parameters of the fit :

• $Q_t = 4,76 \cdot 10^{-15} \text{ C}$, $\Rightarrow \sigma_t = 9,2 \cdot 10^{-2} \text{ mC/m}^2$

• $A = 26 \text{ nm}$

• $Q_p/Z = 2,2 \cdot 10^{-7} \text{ C/m}$

For comparison :

➤ Burnham et al : **diamond/graphite**

• $Q_t = 2 \cdot 10^{-16} \text{ C}$, $\Rightarrow \sigma_t = 4 \cdot 10^{-5} \text{ e/Å}^2$

• $A = 10 \text{ nm}$,

• $Q_p/Z = 4 \cdot 10^{-8} \text{ C/m} \Rightarrow \sigma_p = 8 \cdot 10^{-7} \text{ e/Å}^2$

➤ Sounilhac et al : **tungstene/TiO₂**

• $Q_t = 0,54 \cdot 10^{-15} \text{ C}$

• $A = 68 \text{ nm}$

• charges of the same sign

II.2. Triboelectrification between two similar materials

Modification of the adhesion due to triboelectrification*

Sum up

(1) Instantaneous measurement, Force at low distance (0-100nm) :

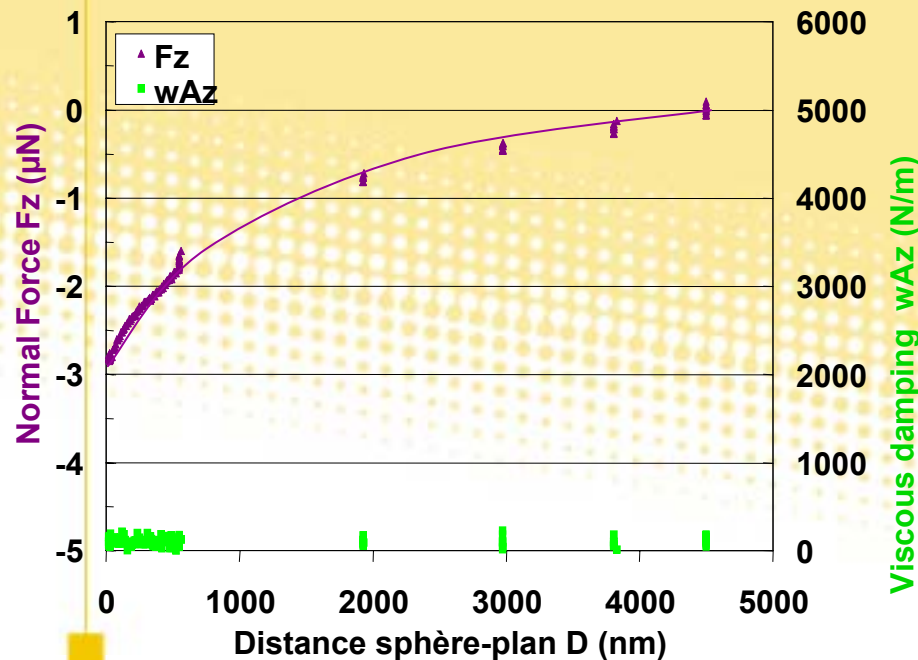
- Adhesion is modified by the presence of an electrostatic force,
- Quantification of the charges (BCP model)
- Charges are mobiles on the surface: $t = 256s$,
- Comparable time with diffusion's times found in the literature on wet alumina surfaces or on polluted one's $\tau \approx 200s$.

II.2. Triboelectrification between two similar materials

Modification of the adhesion due to triboelectrification*

(2) Long time, Force at long distance (1- 5 μ m):

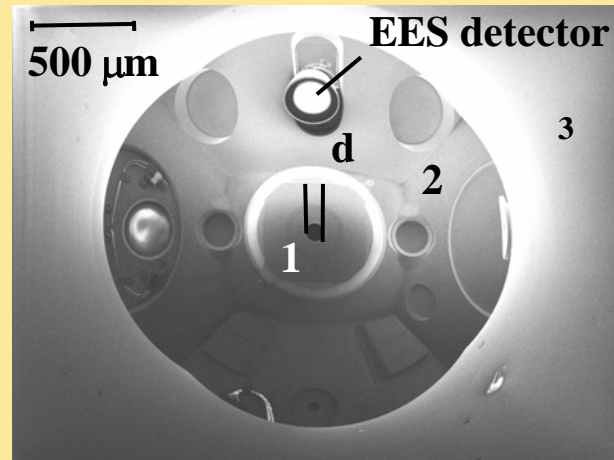
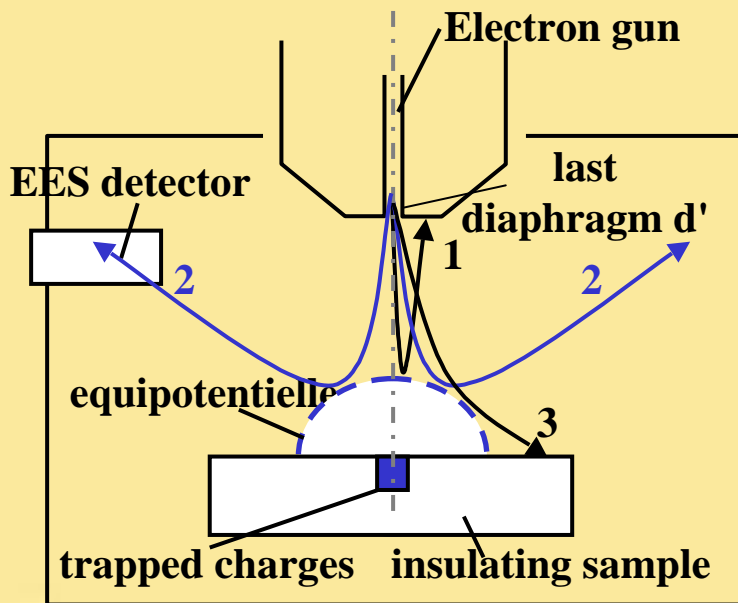
- attraction at long distance in the friction area
- observed on the two types of sphere (smooth or with asperities)
- mesurable several days after the friction test
- charge observed with a SEM



- III. **Characterization of the properties of charges flow and of charges trapping : SEMM method and simulations**
 - 1. "Mirror" method and influence current
 - 2. Simulation of the injection of electrons

III.1. Mirror method and influence current

Mirror method (SEMM)



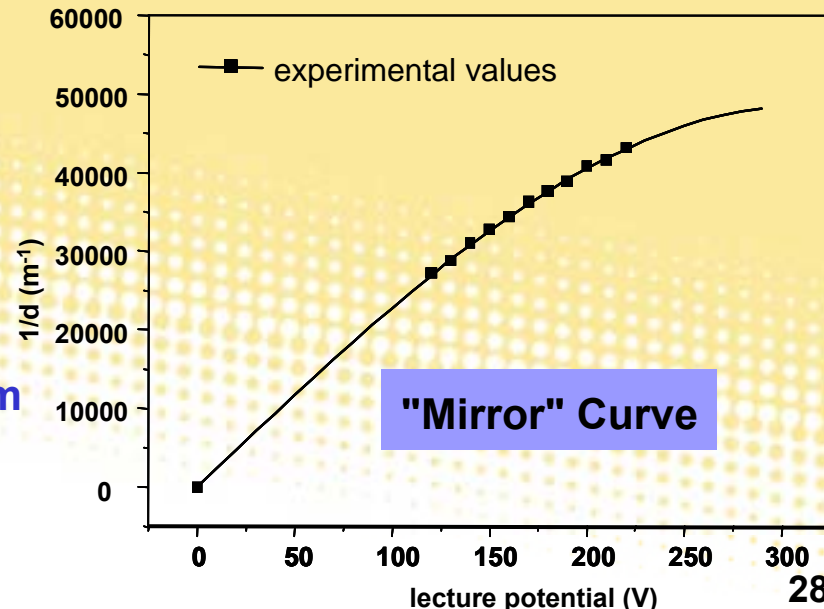
2 Steps:

- injection of high energy electrons (10-30 keV)

→ trapping of charges in the insulator

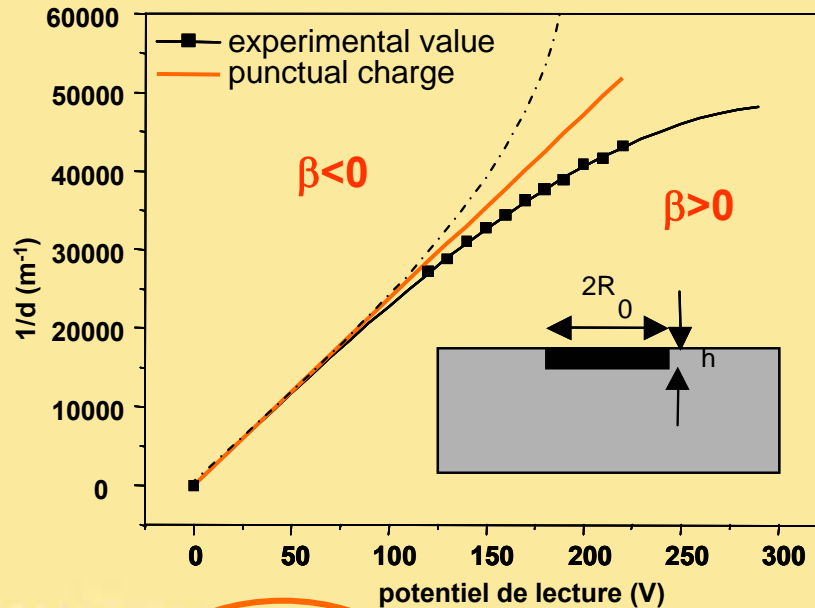
- lecture by a low energy beam (300-1keV)

→ deviation of the electron of the lecture beam



III.1. Mirror method and influence current

Mirror method (SEMM)



Approximation of a punctual charge

$$\frac{1}{d} = \left(\frac{4 \cdot L}{d'} \cdot \frac{1}{A_{\infty} Q_p} \right) \cdot V_i \quad A_{\infty} = \frac{1}{2\pi\epsilon_0(\epsilon_r + 1)}$$

Evaluation of the quantity of trapped charges

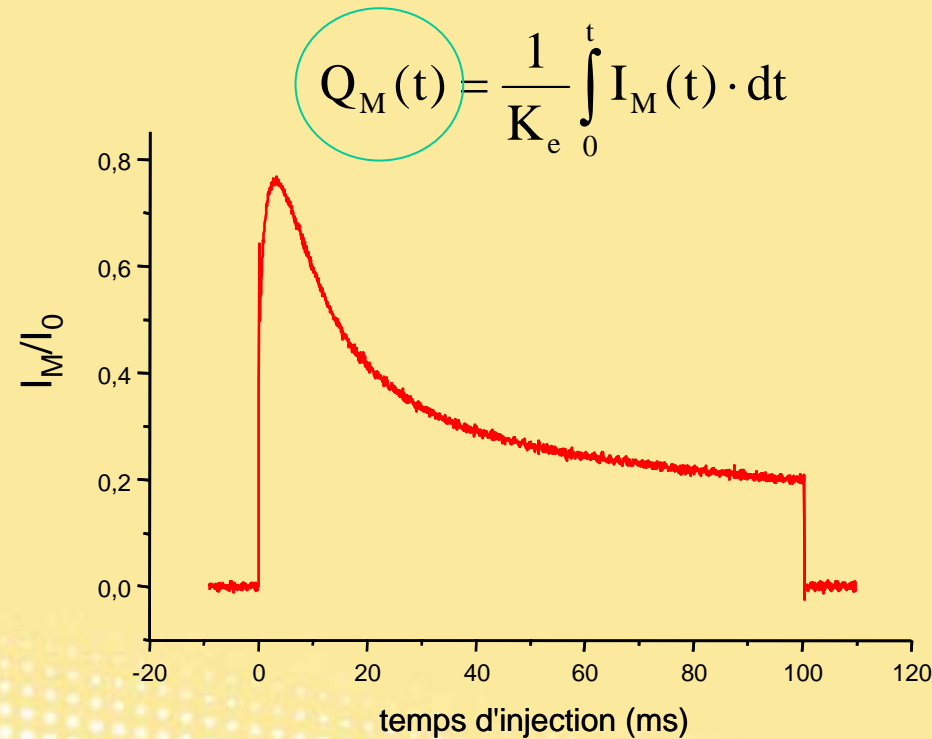
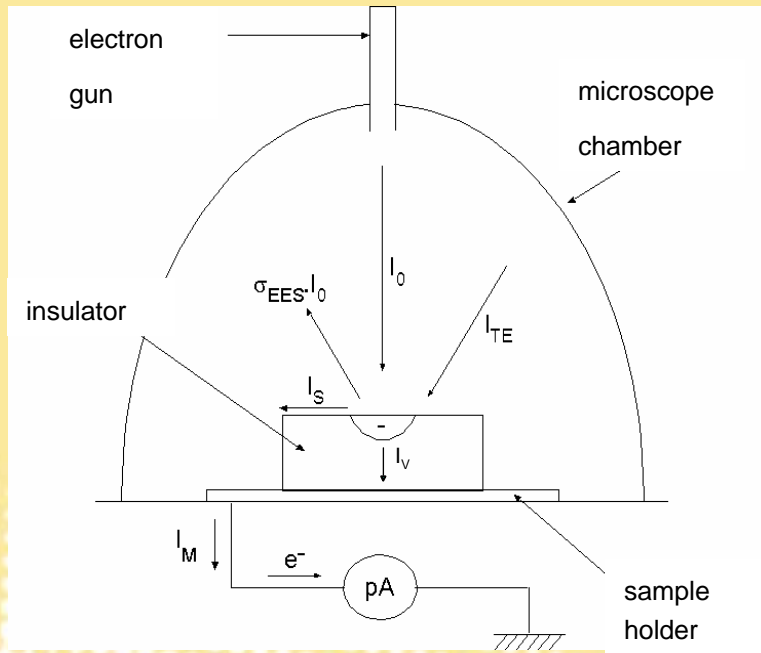
Multipolar development (isotropic material)*

$$\frac{1}{d} = K \left\{ \frac{V}{AQ_p} - 2\beta R_0^2 \left(\frac{V}{AQ_p} \right)^3 \right\}$$

Form of the charges distribution :
 $\beta > 0$: charges on the surface
 $\beta < 0$: charges in the depth

III.1. Mirror method and influence current

Method of the influence current (ICM)



charges injected in the material



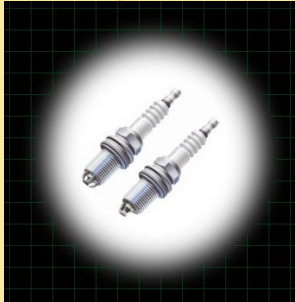
influence charges on the sample holder

$$I_M = (1 - \sigma_{EES}) \cdot I_0 + I_S + I_V + I_{TE}$$

III.1. Mirror method and influence current

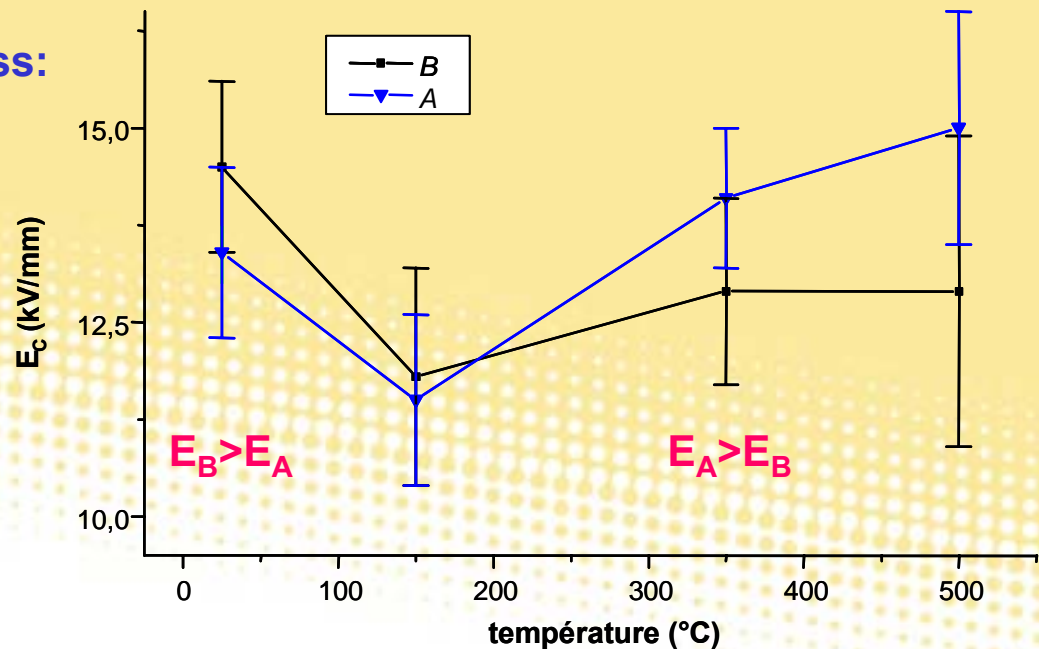
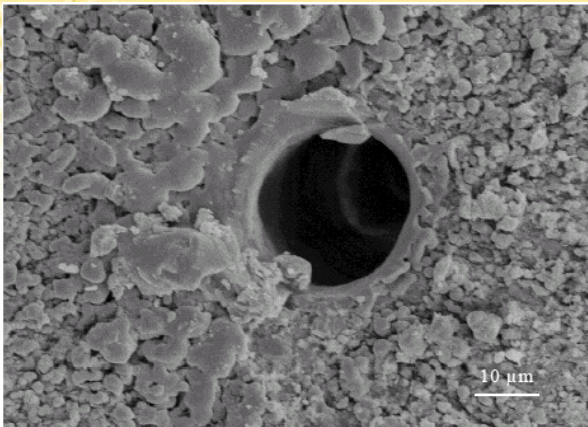
Characterization of polycrystalline alumina samples*

- alumina powder + various sintering aids
- sintering in liquid phase
- example of 2 materials A and B
- ajouts de frittage différents \Rightarrow joints de grains différents



Material	Vitrous Phase (%)
A : Industrial	15,9
B : Laboratory	4,6

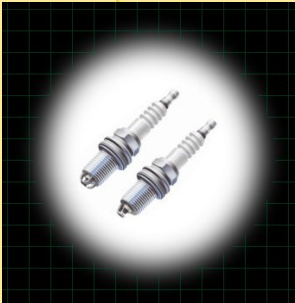
Characterization of the dielectric stiffness:



* X. Meyza, Mémoire de Thèse, D. Goeriot, X. Meyza, M. Touzin, C. Guerret-Piécourt, D. Juvé, D. Tréheux, H.-J. Fitting *Journal of the European Ceramics Society*, (sous presse), Thèse en cours de M. Touzin, St Etienne

III.1. Mirror method and influence current

Characterization of polycrystalline alumina samples*



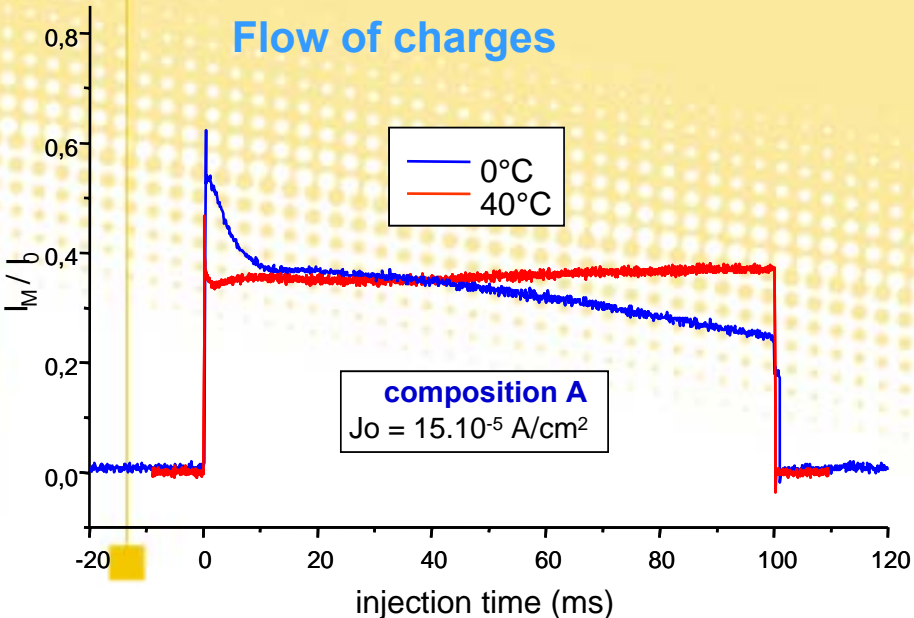
Trapped charge (SEMM)

Stabilization Ratio

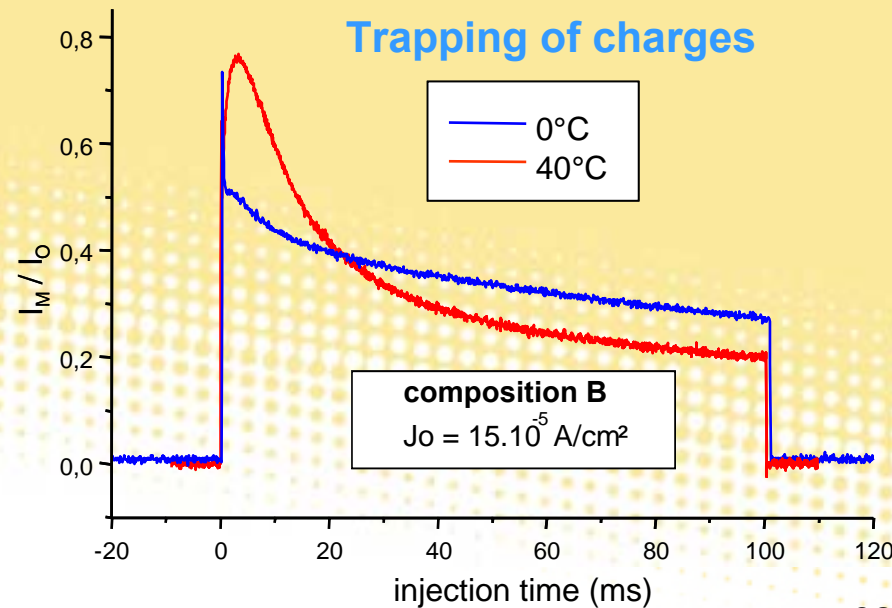
Injected Charge (ICM)

<i>Matériau Industriel (A)</i>	0°C	40°C
Q_P (pC)	94	0
Q_M (pC)	98	108
$R = Q_P / Q_M$	96 %	0
<i>Matériau Laboratoire (B)</i>		
Q_P (pC)	94,5	12,2
Q_M (pC)	105	102
R (%) = Q_P / Q_M	90 %	12 %

Flow of charges

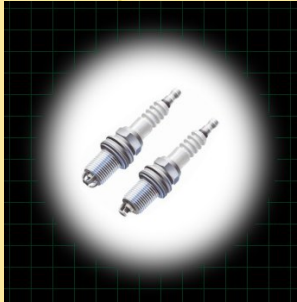


Trapping of charges



III.1. Mirror method and influence current

Characterization of polycrystalline alumina samples*



Effects of the microstructure on the flow and on the trapping of the charges: favorable cases to optimize the dielectric stiffness

At low temperature:

- crystallized secondary phase (material B): deep traps

"Trapping" insulator

At high temperature:

- vitreous secondary phase (material A): traps of weak deepness, favorable to the flow of charges
- weak number of grain joints

"Conductive" Insulator

III.1. Mirror method and influence current

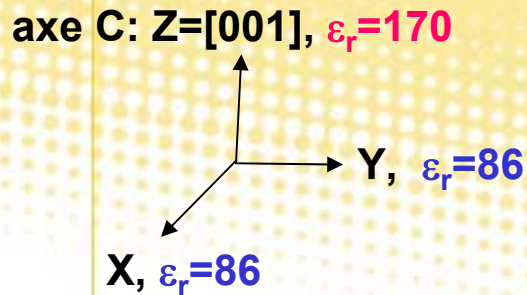
Characterization of a SC with high forbidden gap: TiO₂ rutile*



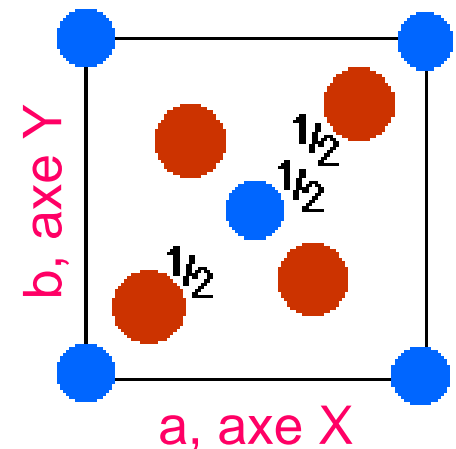
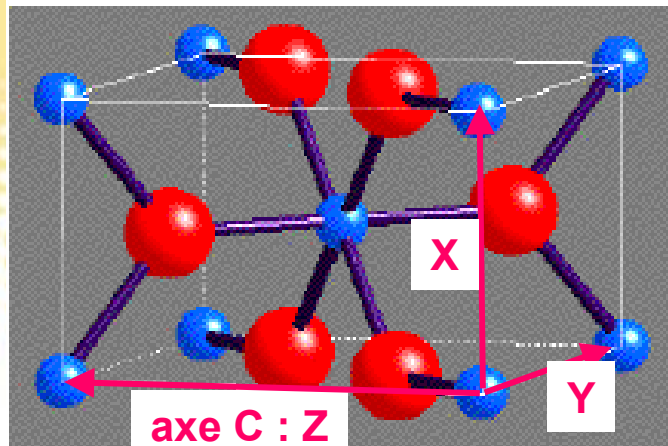
Characteristics of TiO₂ rutile:

- SC with high forbidden gap: 3,1 eV
- resistivity $R > 10^{13} \Omega\text{cm}$ (sensitivity to oxygen)
- anisotropy of the permittivity : $\epsilon_r = 86$ at T_{room} in the X,Y plane
 axe C: $\epsilon_r = 170$ at T_{room} along $Z = [001]$

Structure of TiO₂ rutile



Unit Cell : Tetragonal (a=b, c)



* Temga Temga, Mémoire de Thèse , Lyon, 2004

III.1. Mirror method and influence current

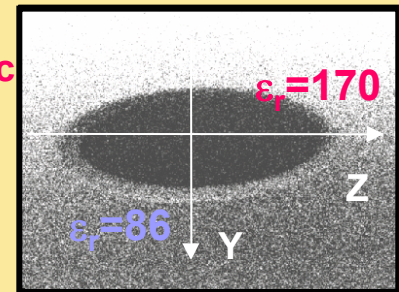
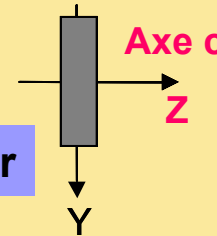
Characterization of a SC with high forbidden gap: TiO_2 rutile*



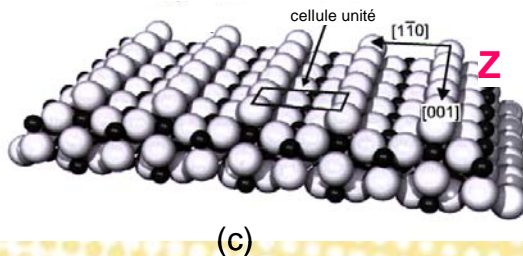
Injection along the axe X= [110]



Anisotropy of the obtained mirror



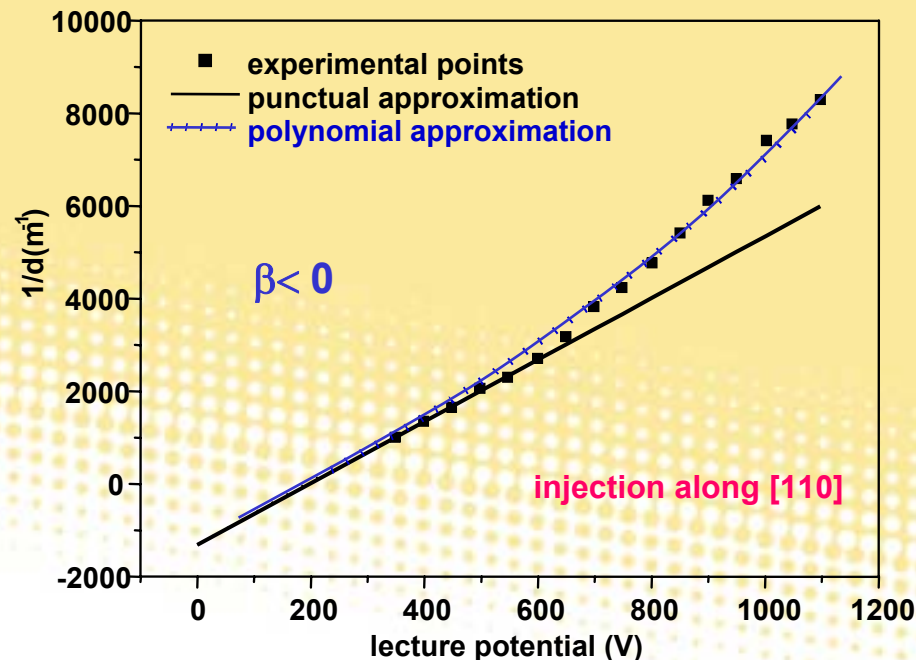
Trapping of the electrons near the Ti ions



Deep trapping :

$$\frac{1}{d} = K \left\{ \frac{V}{AQ_p} - 2\beta R_0^2 \left(\frac{V}{AQ_p} \right)^3 \right\}$$

Cylindrical Distribution radius $R=2\mu\text{m}$
and deepness $h=280\mu\text{m}$



* T. TEMGA, D. JUVE, D. TREHEUX, C. GUERRET-PIECOURT and C. JARDIN soumis à J. Appl. Phys.

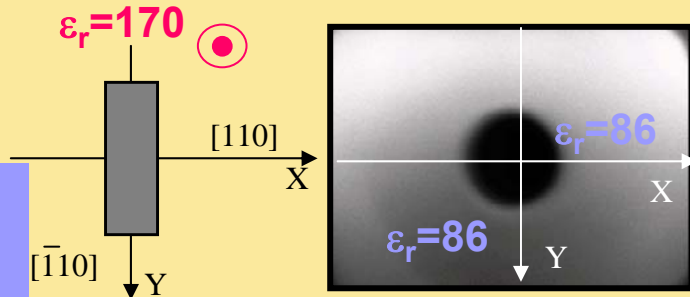
III.1. Mirror method and influence current

Characterization of a SC with high forbidden gap: TiO₂ rutile*

Injection along axe Z= [001]

~~$$\frac{1}{d} = \left(\frac{4 \cdot L}{d'} \cdot \frac{2\pi\epsilon_0(\epsilon_r + 1)}{Q_p} \right) \cdot V_i$$~~

**circular mirror,
analytical model taking into
account the anisotropy of ϵ_r^***

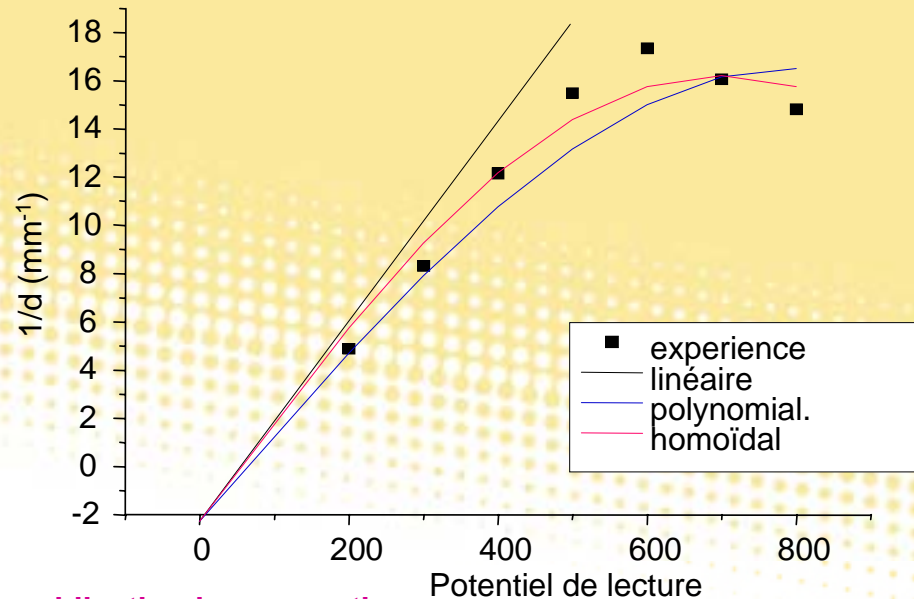


Transversal Isotropic Material: punctual charge

$$\frac{1}{d} = \left(\frac{4 \cdot L}{d'} \cdot \frac{2\pi\epsilon_0 (\sqrt{\epsilon_X} \sqrt{\epsilon_Z} + 1)}{Q_p} \right) \cdot V_i$$

Transversal Isotropic Material: homoïdal distribution

$$\frac{2c}{d} = \frac{4H}{\phi} \left\{ \frac{\sin}{\text{sh}} \right\} \left(\frac{2c \cdot 8\pi\epsilon_0 E_{cin}}{Q} \right)$$



* developed by G DAMAMME, PHDthesis T TEMGA, publication in preparation

III.1. Mirror method and influence current

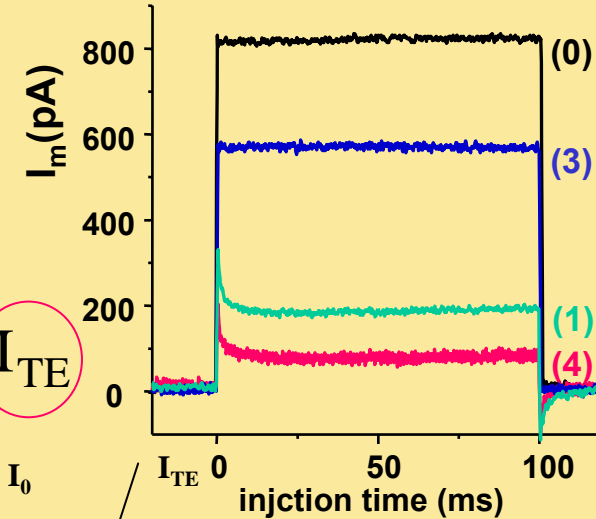
Characterization of a SC with high forbidden gap: TiO₂ rutile*

Importance of leakage current



Modification of the ICM method*

$$I_M = (1 - \sigma_{EES}) \cdot I_0 + I_S + I_V + I_{TE}$$



Metallic guard

I_0

Sample

metallic sample-holder

on/off

(1)

(2)

(3)

Picoammeter

I_{SE}

I_0

I_{TE}

injection time (ms)

Metallic guard

copper disk

I_P

I_C

I_{TE}

Mica sheet

Metallic Sample Holder

I_g

Picoam
meter

Montage 4

Picoam
meter

* T. Temga, C. Guerret-Piécourt, D. Juvé, D. Trégeux, C. Jardin, (2003) An. Rep. CEIDP, Albuquerque, p 221-224

** proposition HJ Fitting,

- III. **Characterization of the properties of charges flow and of charges trapping : SEMM method and simulations**
 - 1. "Miror" method and influence current
 - 2. Simulation of the injection of electrons

III.2. Simulation of the injection of electrons*

Self-consistent model

Injection of high energetic electrons in an insulator**:

- backscattered electrons η
- penetration in the bulk PE
- generation of e-h pairs (secondary e)
- secondary emission
- e-h recombination
- trapping, effect of the electric field

Principle of the simulation:

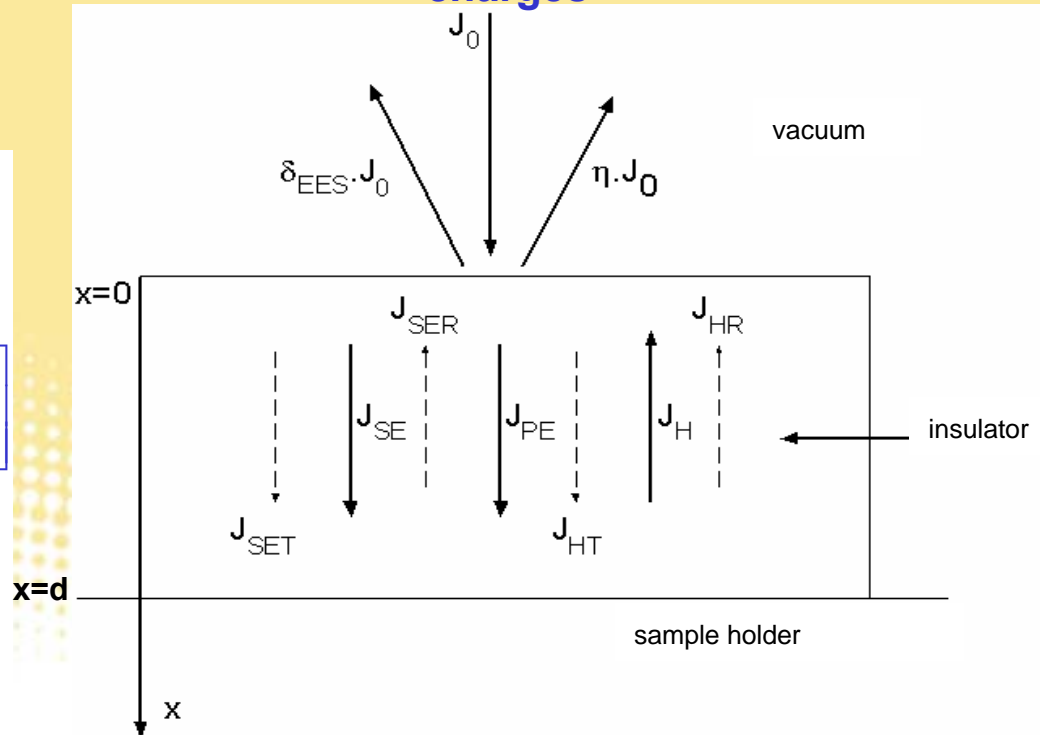
- model with 1 dimension
- determination for each time and for each position x in the sample of the quantity of charges

$$j_{PE}(x, E) = j_0(1-\eta) \exp \left[-4.605 \left(\frac{x}{R(E, z)} \right)^{p(z)} \right]$$

$$g_i / \text{\AA} = 0.146 \cdot (E_0 / \text{keV})^{-0.3} \exp \left[-7.5 \left(\frac{x}{R} - 0.3 \right)^2 \right]$$

$$j_T^R(x) = \left[j_T^R(x \pm \Delta x) + \frac{1}{2} j_0 g_i(x) \Delta x \right] \cdot W(x)$$

$$j(x) = -j_{PE}(x) - j_{ET}(x) + j_{ER}(x) + j_{HT}(x) - j_{HR}(x)$$



* Collaboration with Pr HJ Fitting, University of Rostock, PHDThesis X Meyza, C Dutriez, and M Touzin

** H.J. Fitting, Phys. Status solid (a), 1974. 26 . I.A..Glavatskikh , V.S. Kortov, H.-J. Fitting, J. Appl. Phys., 2001. 89(2)

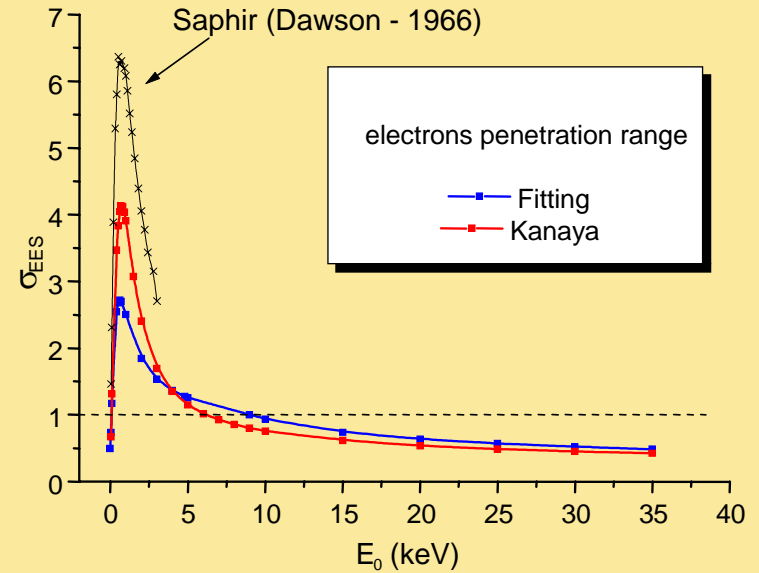
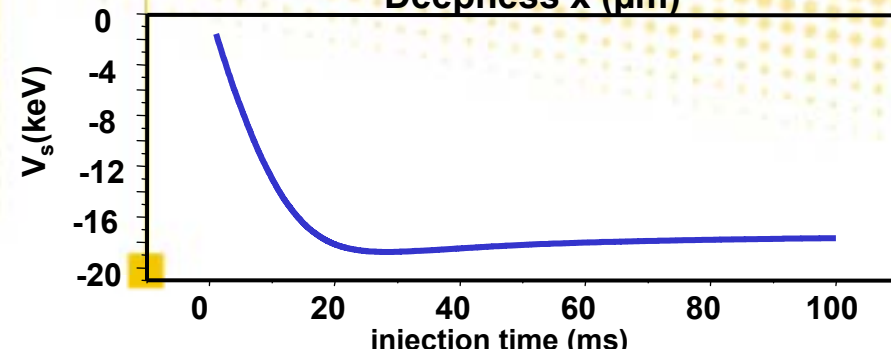
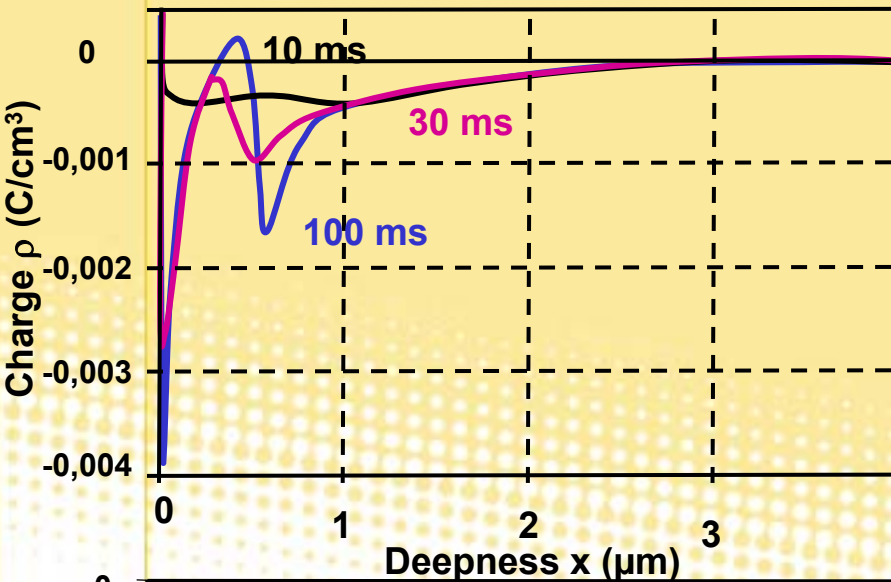
III.2. Simulation of the injection of electrons*



Self-consistent model

Very short injection:

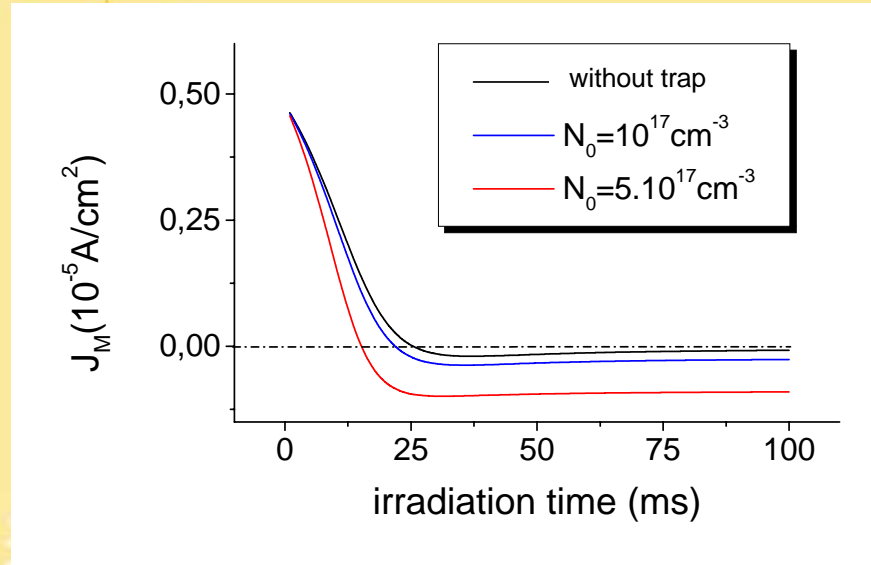
- determination of the instantaneous secondary emission curve (negligible V_s)
- validation of the model



Self-regulated Phenomenon:
 negatives charges are injected in the depth of the sample leading to the creation of a high negative potential and increase de secondary emission incoming charges are slow down less and less charges are injected, surface potential and secondary emission become stable

III.2. Simulation of the injection of electrons*

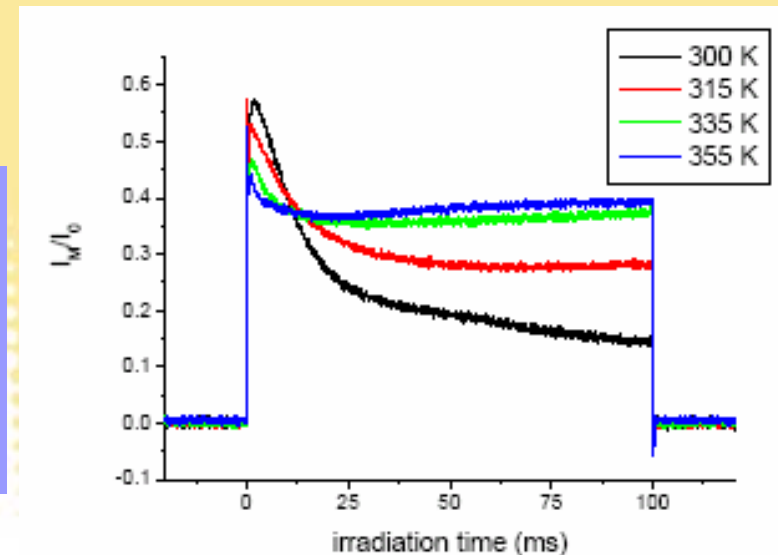
Self-consistent Model



**Example of simulation:
effect of the electronic traps number on
the decrease of the influence current**

Development of a new model* :

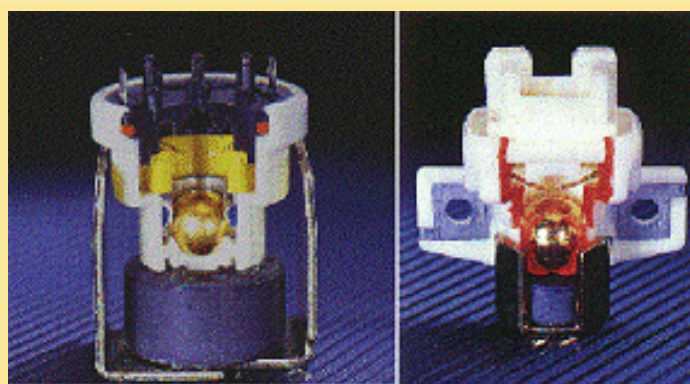
- to take into account the effect of the temperature through the Poole-Frenkel effect
- to take into account the anisotropy of the diffusion and drift due to the field



* Collaboration with Pr HJ Fitting, University of Rostock, PHDThesis C Dutriez, and M Touzin

IV. **Conclusions and Prospects**

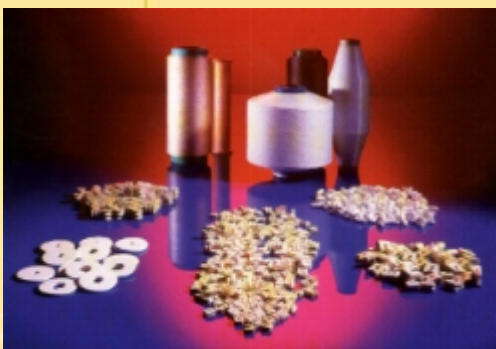
Importance of the triboelectrification



Electromechanical sensor of acceleration for airbag



Pieces for mitigation tap

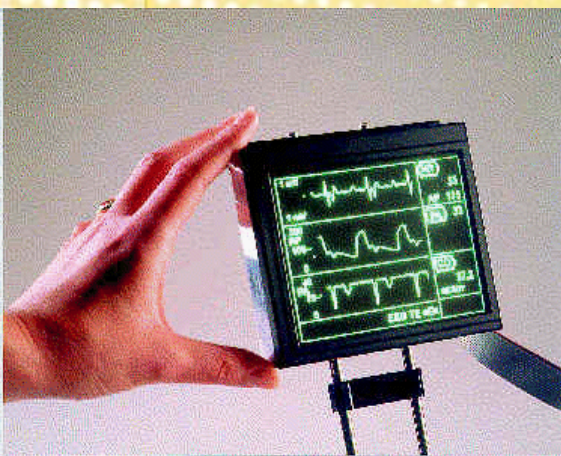


yarn-guide

Evidencing of the importance of the electrical charges for the properties of friction and adhesion

Understanding of the mechanisms of injection and trapping of the electrical charges :

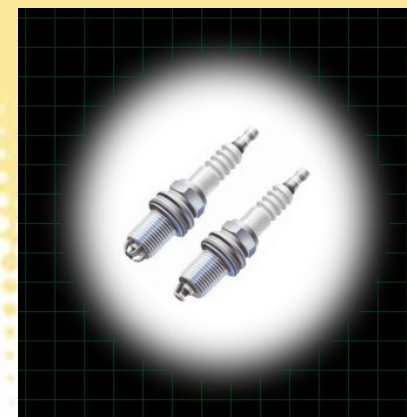
- experiments
- simulation



FEG screen

Improvement of the dielectric strength by determination of the structural parameters leading to a better accommodation of the injected charges depending on the temperature of use :

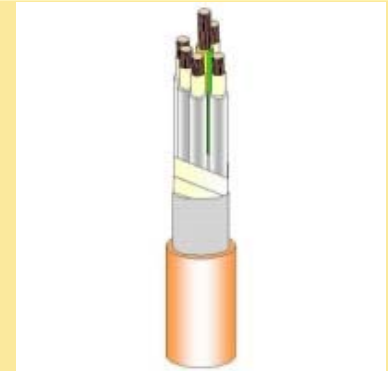
- "trapping" insulators or
- "conductive" insulators



Sparkling plug

IV.2. Prospects : The polymers insulators

- Study of the trapping and flow of electrical charges in the polymers*
- Link between triboelectrification of the melt and emergence of defects during the extrusion of molten polymers**
- Utilization of ICM and SEMM methods to characterize the nanostructured materials
- Study of polymers/ conductive charges composites: CNT-Elastomers, PANI- BuA...***



* Thèse Cédric Dutriez, C. Dutriez, X. Meyza, C. Guerret-Piécourt, D. Tréheux, H.J. Fitting (2003) Annual Report Conf. on Elect. Insul.Dielect. Phenomena, Albuquerque, 2003, p 530-533

** Thèse F. Flores, S. Tonon, A. Lavernhe-Gerbier, F. Flores, A. Allal, C. Guerret-Piécourt J. of Non-Newtonian Fluid Mechanics, (accepté, sous presse)

*** 1 brevet déposé, V. Datsyuk, C. Guerret-Piécourt, S. Dagréou, L. Billon, J.-C. Dupin, E. Flahaut, A. Peigney, C. Laurent Carbon (sous presse)

**Sandrine BEC, Gilles DAMAMME , Vitaliy DATSYUK, Cédric DUTRIEZ,
Hans-Joachim FITTING, Fabrice FLORES, Dominique GOEURIOT,
Denyse JUVÉ, Xavier MEYZA, Olivier GUERRET, Fabrice SEGALT, Temga TEMGA,
André TONCK, Sébastien TONON, Matthieu TOUZIN , Daniel TRÉHEUX .../...**

...

- **Laboratoire des Solides Irradiés (SESI) à l'Ecole Polytechnique**
- **Laboratoire d'Analyse et d'Architecture des Systèmes à Toulouse**
- **Laboratoire de Tribologie et de Dynamique des Systèmes de l'ECLyon**
- **Laboratoire d' Ingénierie et Fonctionnalisation des Surfaces de l'ECLyon**
- **Laboratoire de Physico-Chimie des Polymères de Pau**